

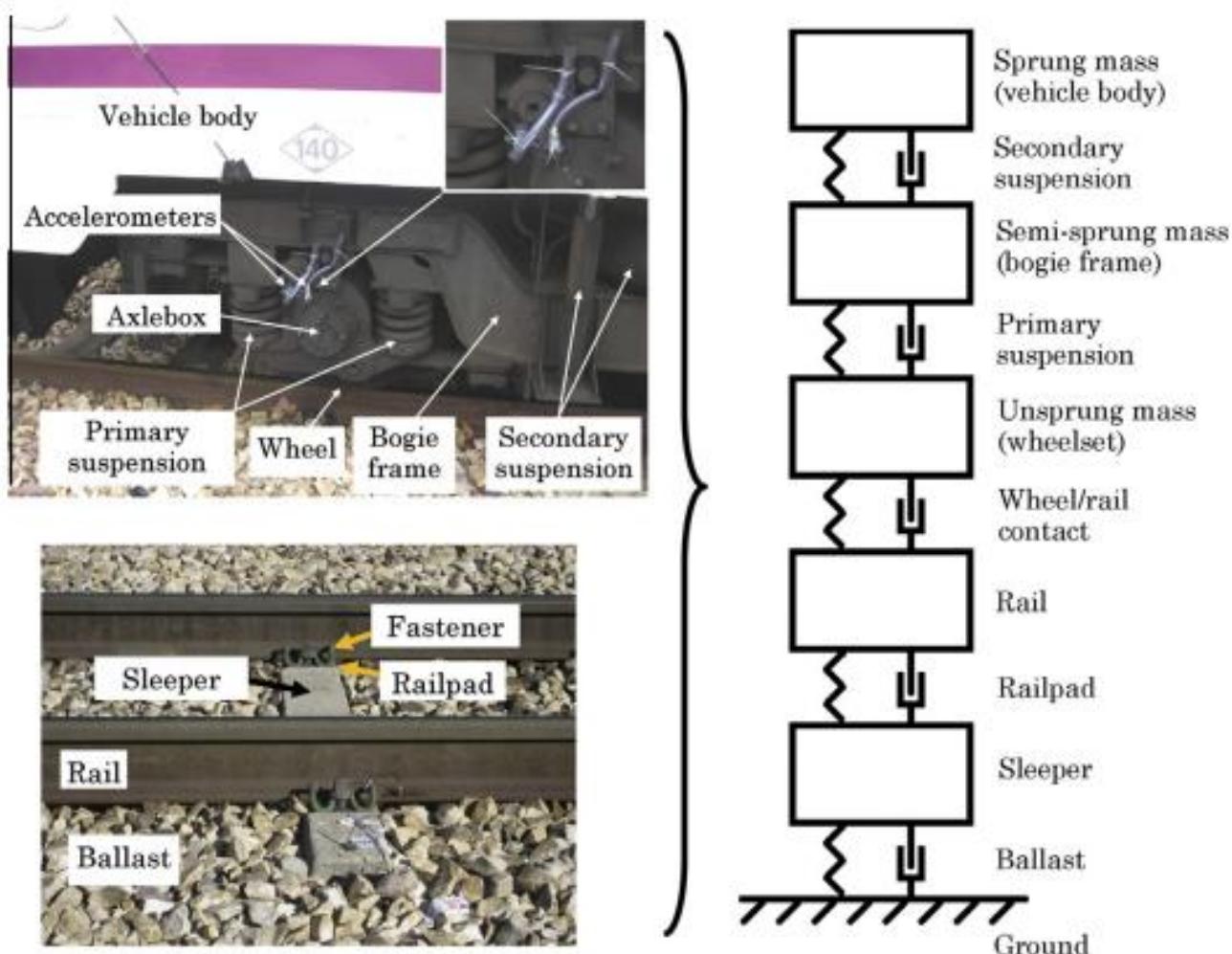
Time Frequency Analysis of Railway Polygonized Wheel Detection

2022.12.6

Outline

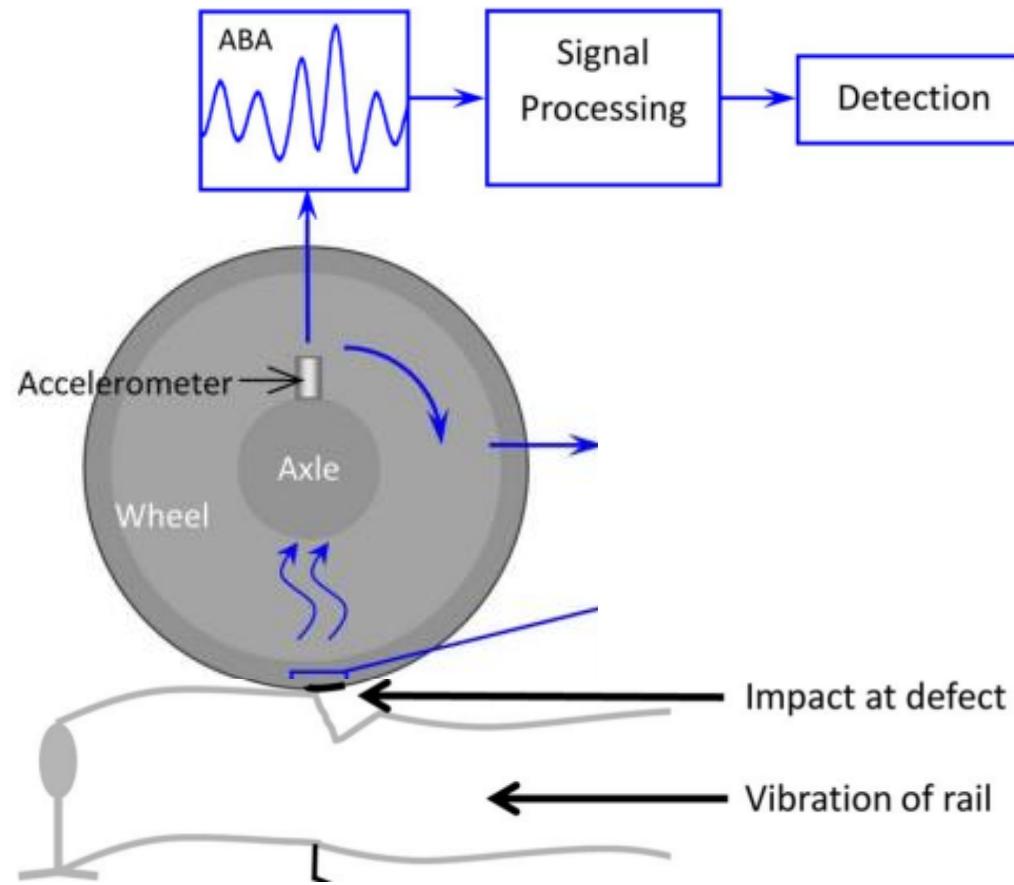
- ▶ Introduction
 - ▶ How to Measure
 - ▶ Polygonized Wheel
- ▶ Method
 1. Adaptive Noise Cancellation (ANC)
 2. Ensemble EMD + Wigner-Ville Distribution
- ▶ Results
- ▶ Reference

How to Measure?

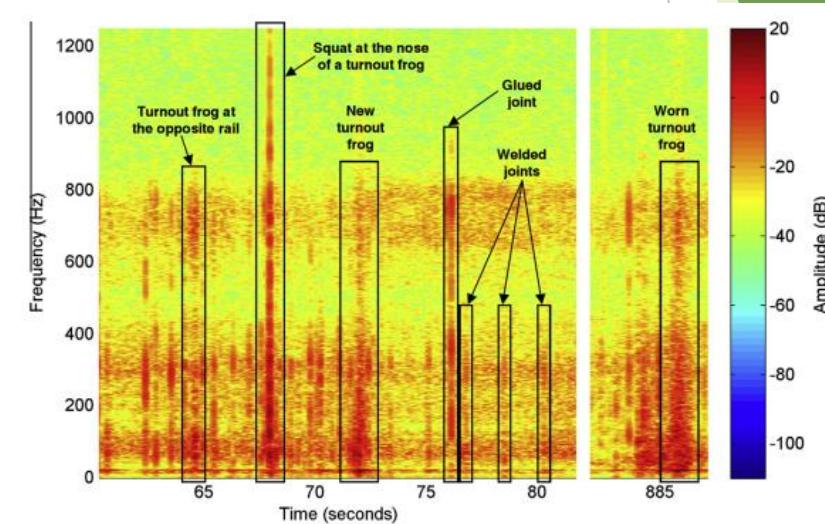


From Reference [2]

How to Measure?

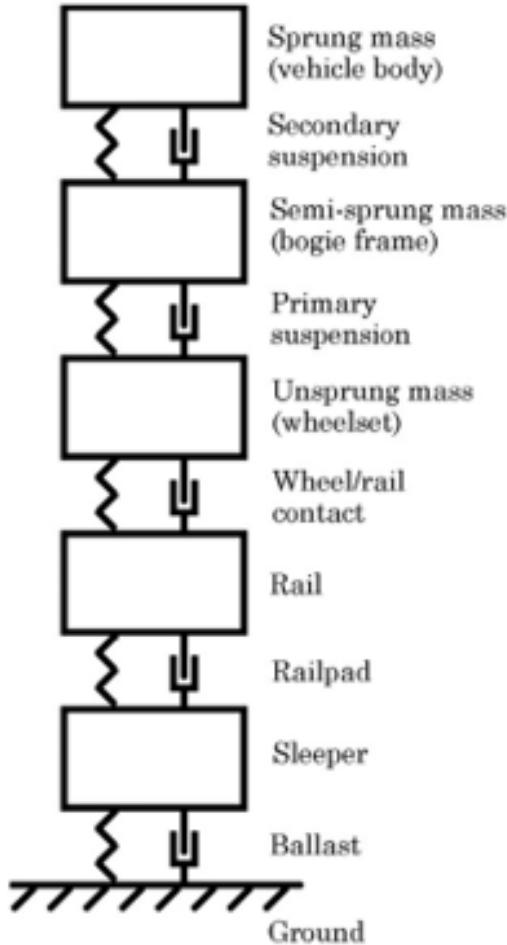


From Reference [3]

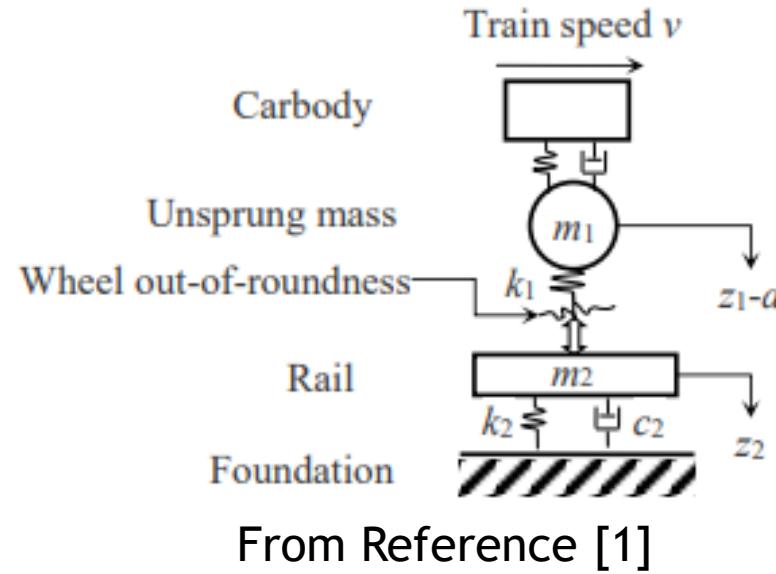


From Reference [2]

Polygonized Wheel

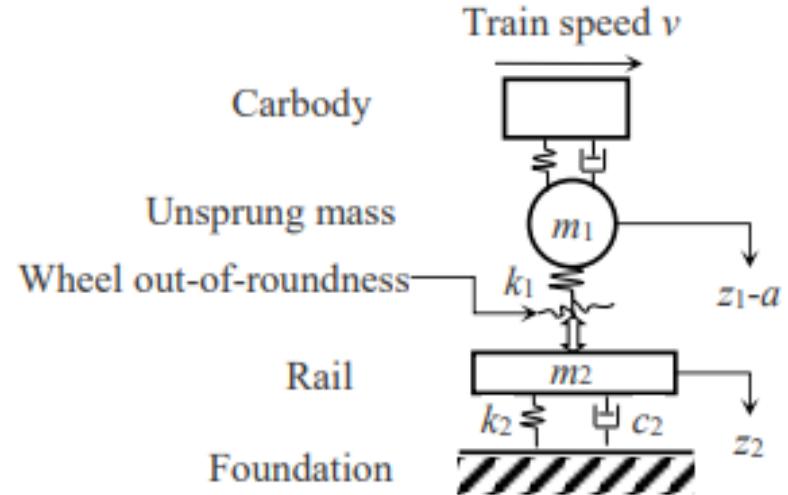


From Reference [2]



From Reference [1]

Polygonized Wheel



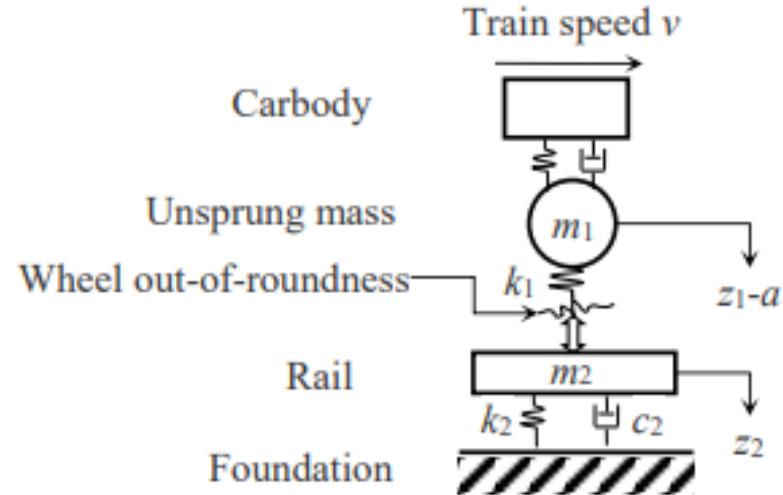
z_1 : vertical displacement of wheel set k_1

z_2 : vertical displacement of the track

a : out-of-roundness amplitude

$$\begin{cases} m_1 \ddot{z}_1 + k_1(z_1 - a - z_2) = 0 \\ m_2 \ddot{z}_2 + c_2 \dot{z}_2 + k_2 z_2 - k_1(z_1 - a - z_2) = 0 \end{cases}$$

Polygonized Wheel



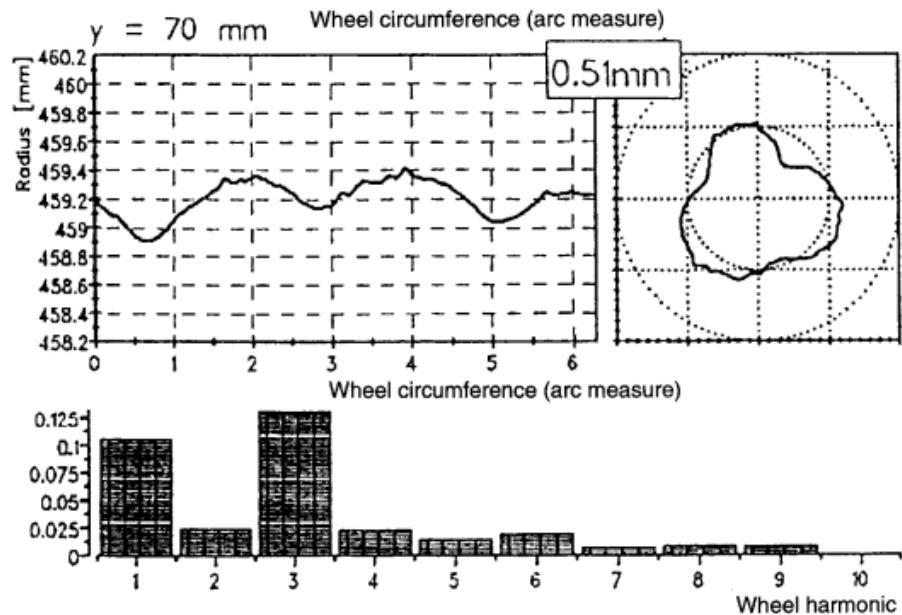
z_1 : vertical displacement of wheel set k_1
 z_2 : vertical displacement of the track
a: out-of-roundness amplitude

$$\begin{cases} m_1 \ddot{z}_1 + k_1(z_1 - a - z_2) = 0 \\ m_2 \ddot{z}_2 + c_2 \dot{z}_2 + k_2 z_2 - k_1(z_1 - a - z_2) = 0 \end{cases}$$

$$\Rightarrow \begin{cases} \frac{\ddot{z}_1}{\omega_1^2} + z_1 - z_2 = a \\ \frac{\ddot{z}_2}{\omega_2^2} + \frac{c_2}{k_1} \dot{z}_2 + \left(\frac{k_1 + k_2}{k_1} \right) z_2 - z_1 = -a \end{cases}$$

where $\omega_1 = \sqrt{k_1/m_1}$ and $\omega_2 = \sqrt{k_2/m_2}$

Polygonized Wheel



From Reference [4]

- z_1 : vertical displacement of wheel set k_1
 z_2 : vertical displacement of the track
a: out-of-roundness amplitude

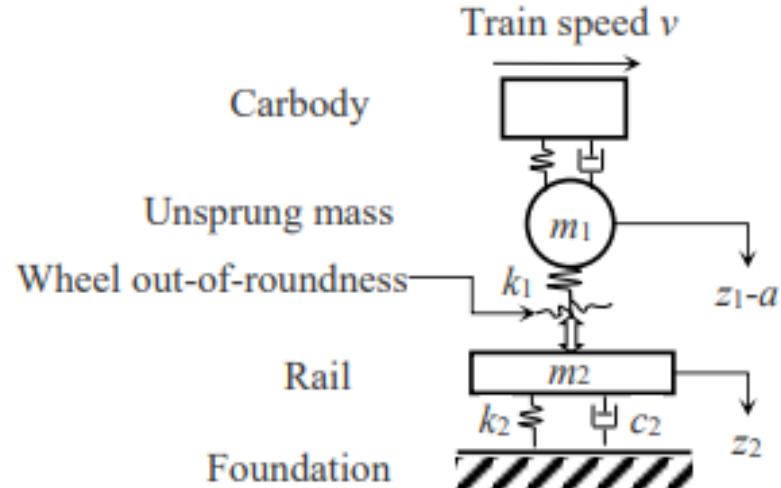
$$a \rightarrow a(t) = a \sin(\omega t + \varphi)$$

Laplace transform:

$$a(s) = \frac{a(s \sin \theta + \omega \sin \theta)}{s^2 + \omega^2}$$

$$\begin{cases} z_1(s) = H_{z1}(s)a(s) \\ z_2(s) = H_{z2}(s)a(s) \end{cases}$$

Polygonized Wheel



z_1 : vertical displacement of wheel set k_1
 z_2 : vertical displacement of the track
a: out-of-roundness amplitude

Laplace transform of the solution:

$$\begin{cases} \left(\frac{s^2}{\omega_1^2} + 1\right)z_1(s) - z_2(s) = a(s) \\ z_1(s) - \left(\frac{s^2}{\omega_2^2} + \frac{c_2 s}{k_1} + \frac{k_2}{k_1} + 1\right)z_2(s) = a(s) \end{cases}$$

$$H_{z1}(s) = \frac{z_1(s)}{a(s)} = \frac{\frac{s^2}{\omega_2^2} + \frac{c_2 s}{k_1} + \frac{k_2}{k_1}}{\frac{s^4}{\omega_1^2 \omega_2^2} + \frac{c_2 s^3}{k_1 \omega_1^2} + \left[\frac{1}{\omega_2^2} + \left(\frac{k_2}{k_1} + 1\right) \frac{1}{\omega_1^2}\right] s^2 + \frac{c_2 s}{k_1} + \frac{k_2}{k_1}}$$

Polygonized Wheel

$$H_{z1}(s) = \frac{\frac{s^2}{\omega_2^2} + \frac{c_2 s}{k_1} + \frac{k_2}{k_1}}{\frac{s^4}{\omega_1^2 \omega_2^2} + \frac{c_2 s^3}{k_1 \omega_1^2} + \left[\frac{1}{\omega_2^2} + \left(\frac{k_2}{k_1} + 1 \right) \frac{1}{\omega_1^2} \right] s^2 + \frac{c_2 s}{k_1} + \frac{k_2}{k_1}}$$

$$\ddot{z}_1(s) = s^2 z_1(s) = s^2 H_{z1}(s) a(s) = s^2 H_{z1}(s) \frac{a(s \sin \theta + \omega \sin \theta)}{s^2 + \omega^2}$$

$$\ddot{z}_1(s) = \frac{\frac{s^4}{\omega_2^2} + \frac{c_2 s^3}{k_1} + \frac{k_2}{k_1} s^2}{\frac{s^4}{\omega_1^2 \omega_2^2} + \frac{c_2 s^3}{k_1 \omega_1^2} + \left[\frac{1}{\omega_2^2} + \left(\frac{k_2}{k_1} + 1 \right) \frac{1}{\omega_1^2} \right] s^2 + \frac{c_2 s}{k_1} + \frac{k_2}{k_1}} \frac{a(s \sin \theta + \omega \sin \theta)}{s^2 + \omega^2}$$

Routh-criterion

For a fourth-order polynomial $P(s) = a_4s^4 + a_3s^3 + a_2s^2 + a_1s^1 + a_0$, if

1. All the coefficients $a_i > 0$
2. $a_3a_2a_1 > a_4a_1^2 + a_3^2a_0$
3. $a_3a_2 > a_4a_1$

Then $P(s)$ is stable.

Therefore, $\frac{s^4}{\omega_1^2\omega_2^2} + \frac{c_2s^3}{k_1\omega_1^2} + \left[\frac{1}{\omega_2^2} + \left(\frac{k_2}{k_1} + 1 \right) \frac{1}{\omega_1^2} \right] s^2 + \frac{c_2s}{k_1} + \frac{k_2}{k_1}$ is stable.

Polygonized Wheel

$$H_{z1}(s) = \frac{\frac{s^2}{\omega_2^2} + \frac{c_2 s}{k_1} + \frac{k_2}{k_1}}{\frac{s^4}{\omega_1^2 \omega_2^2} + \frac{c_2 s^3}{k_1 \omega_1^2} + \left[\frac{1}{\omega_2^2} + \left(\frac{k_2}{k_1} + 1 \right) \frac{1}{\omega_1^2} \right] s^2 + \frac{c_2 s}{k_1} + \frac{k_2}{k_1}}$$

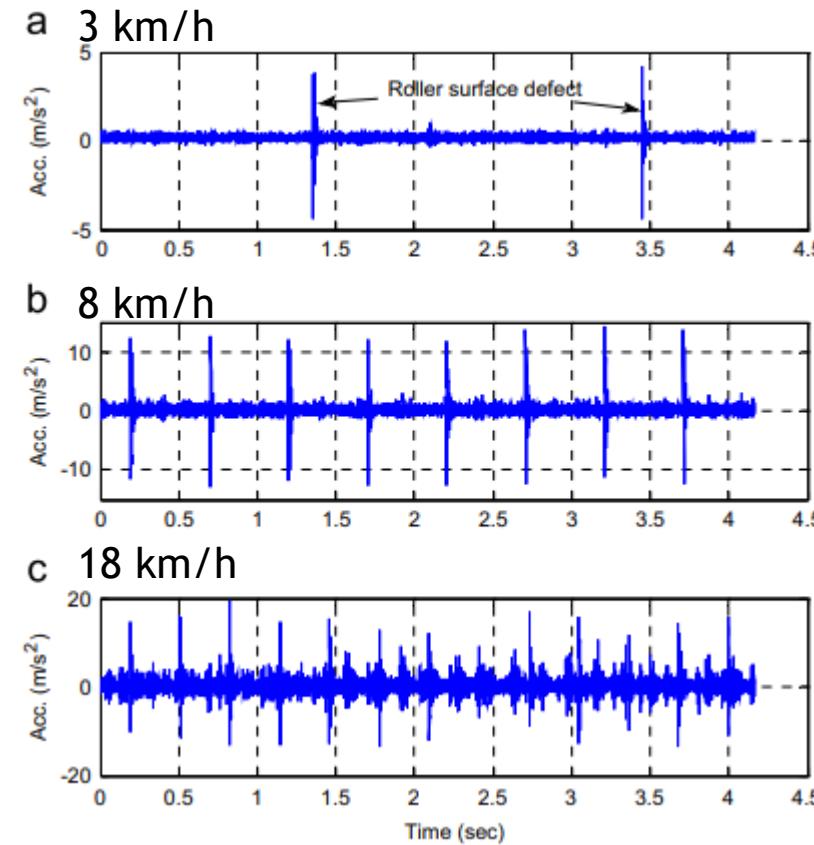
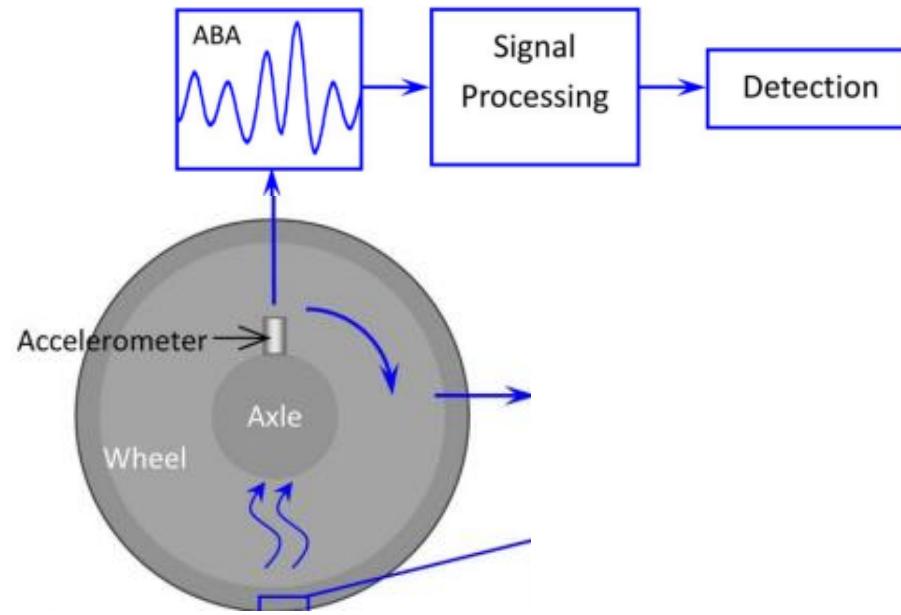
$$\ddot{z}_1(s) = s^2 z_1(s) = s^2 H_{z1}(s) a(s) = s^2 H_{z1}(s) \frac{a(s \sin \theta + \omega \sin \theta)}{s^2 + \omega^2}$$

Since $\frac{s^4}{\omega_1^2 \omega_2^2} + \frac{c_2 s^3}{k_1 \omega_1^2} + \left[\frac{1}{\omega_2^2} + \left(\frac{k_2}{k_1} + 1 \right) \frac{1}{\omega_1^2} \right] s^2 + \frac{c_2 s}{k_1} + \frac{k_2}{k_1}$ is stable by Routh-criterion,
the necessary and sufficient for all roots having negative real parts is

$$\ddot{z}_1(s) = \sum_{i=1}^4 \frac{A_i}{s + p_i} + \frac{Bs + C}{s^2 + \omega^2}$$

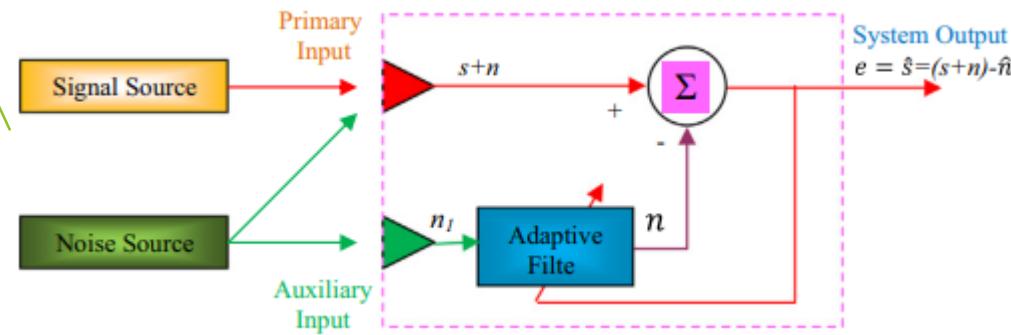
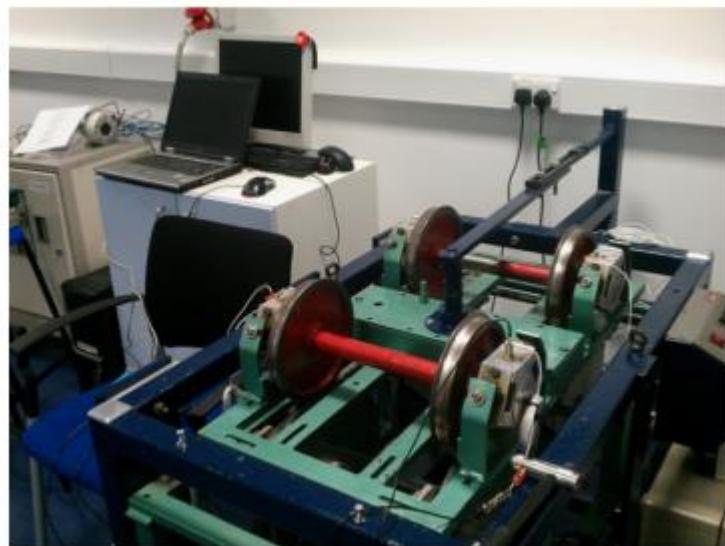
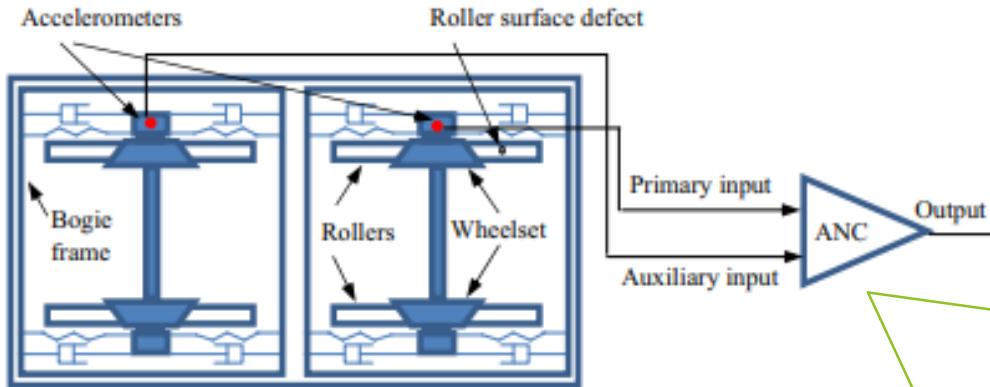
$$\ddot{z}_1 = \sum_{i=1}^4 A_i e^{-p_i t} + D \cos(\omega t + \varphi)$$

Adaptive Noise Cancellation

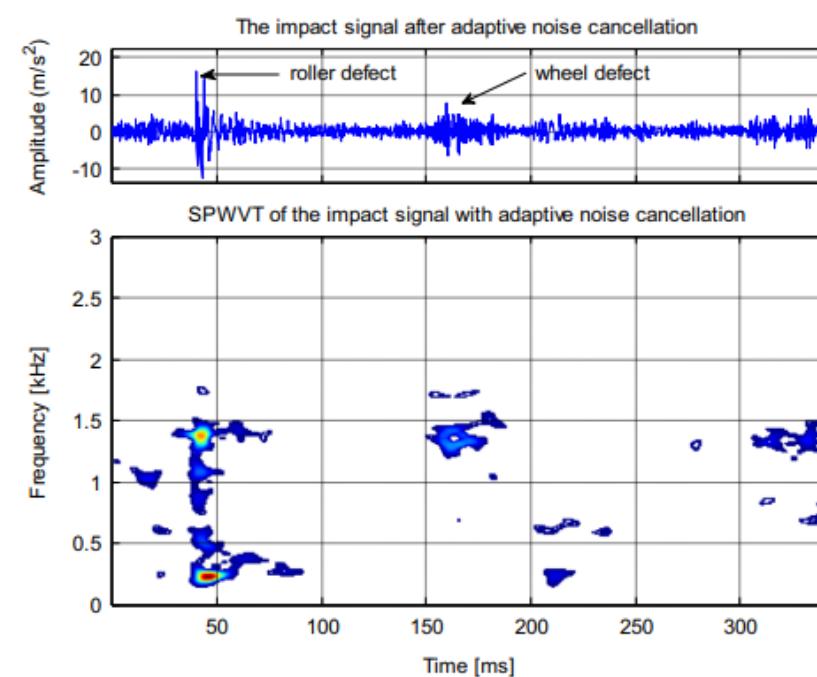
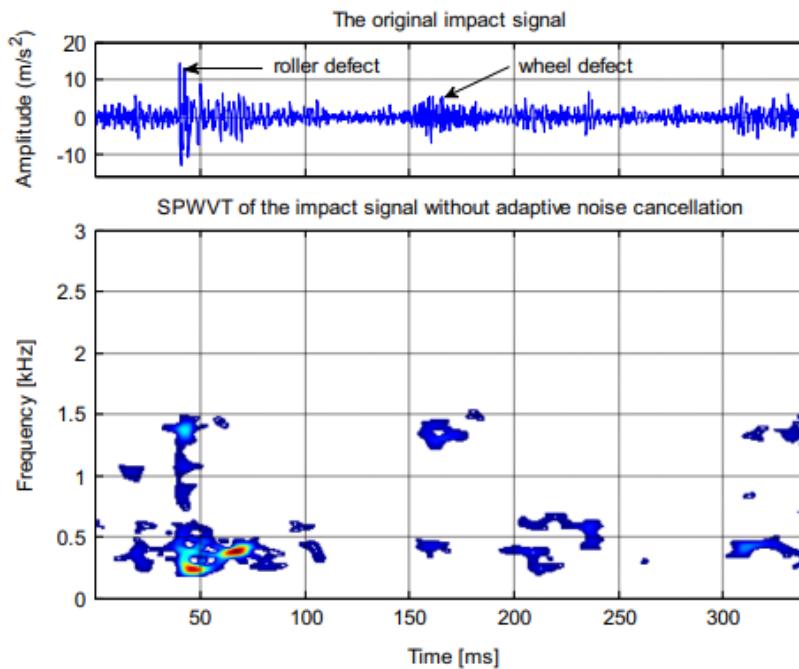


From Reference [5]

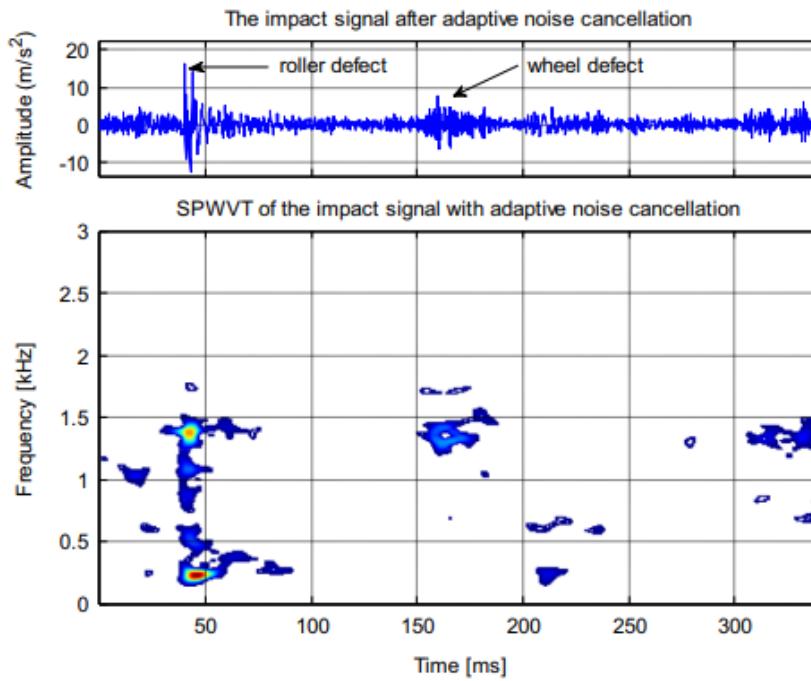
Adaptive Noise Cancellation



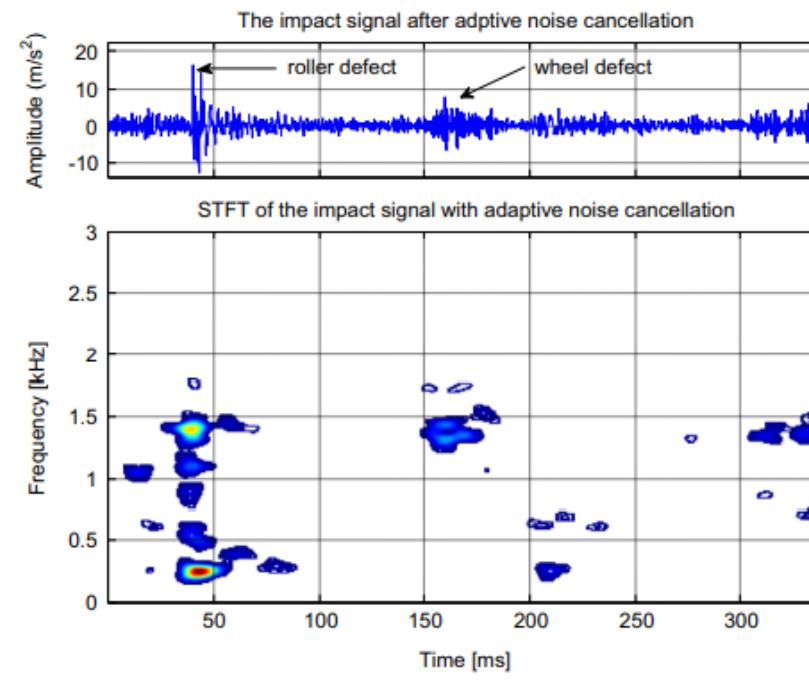
Adaptive Noise Cancellation



Wigner-Ville Distribution

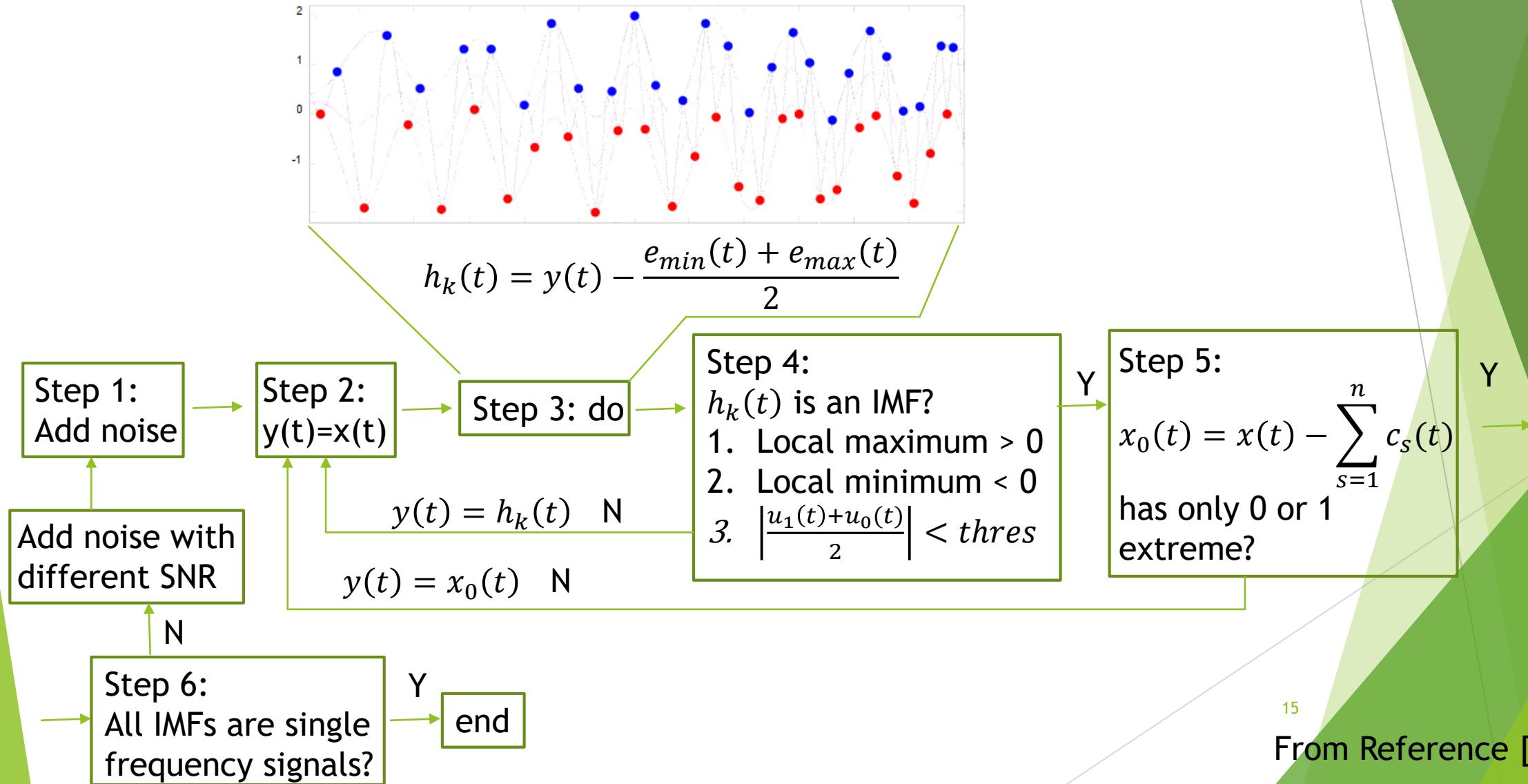


$$\int_{-\infty}^{\infty} s(t+\tau/2)s^*(t-\tau/2)e^{-j\omega\tau}d\tau$$

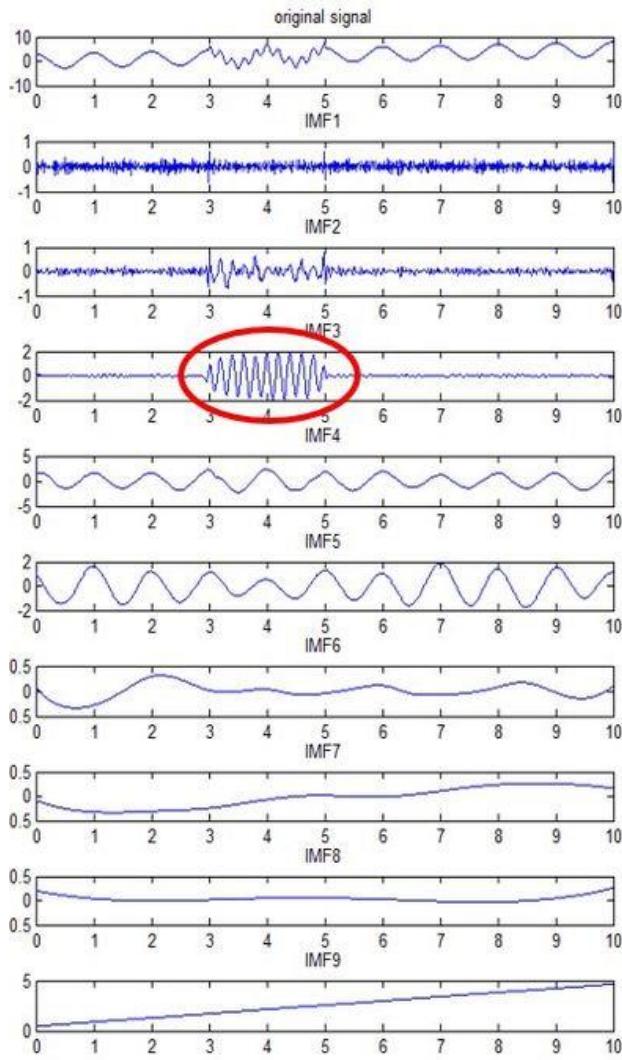


$$\int_{-\infty}^{\infty} h(\tau-t)s(t)e^{-j\omega t}dt$$

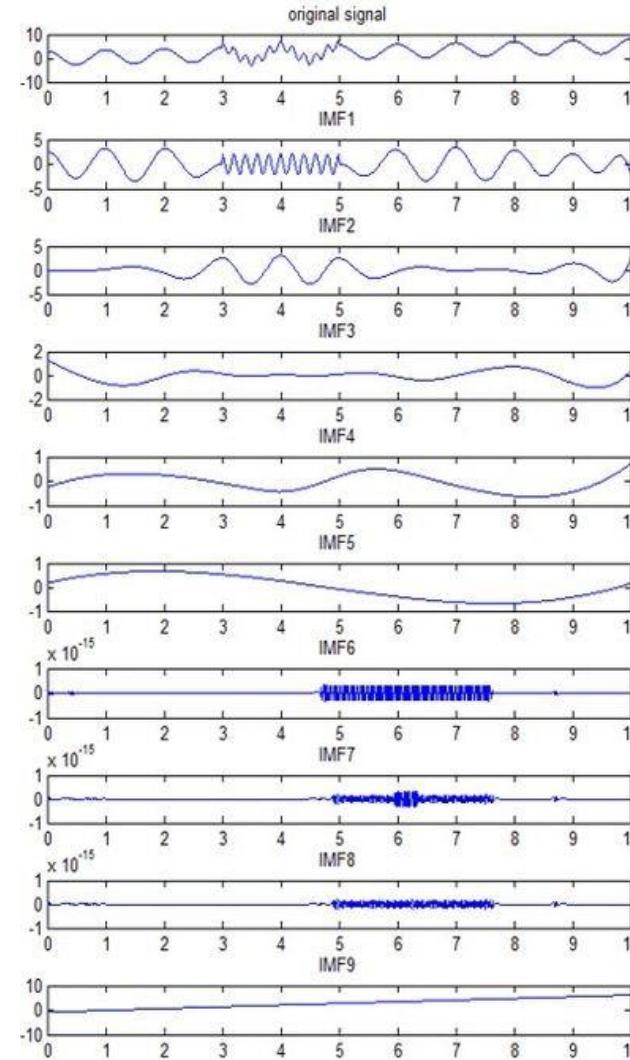
Ensemble EMD



Ensemble EMD

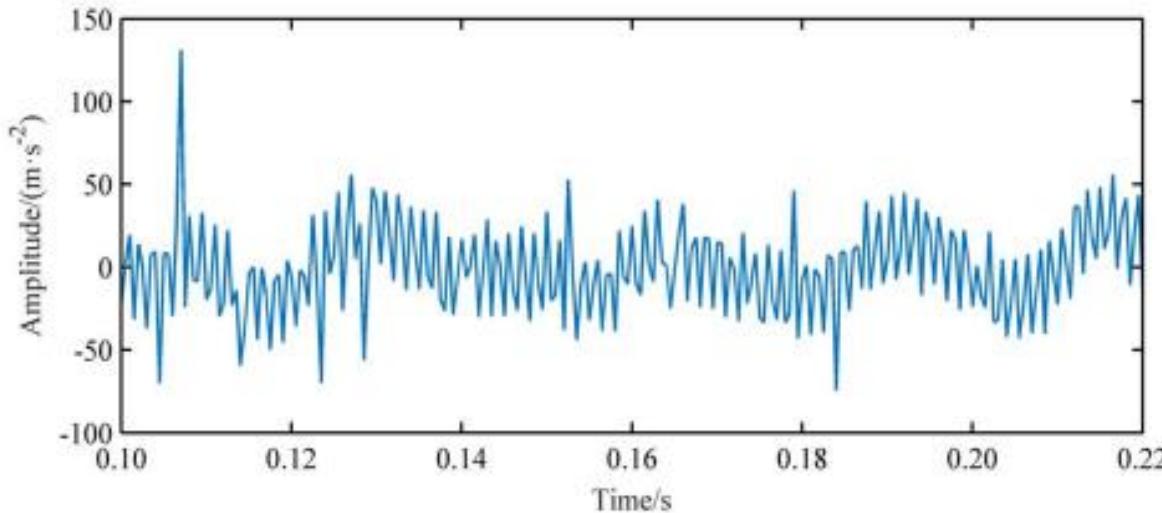


Ensemble EMD



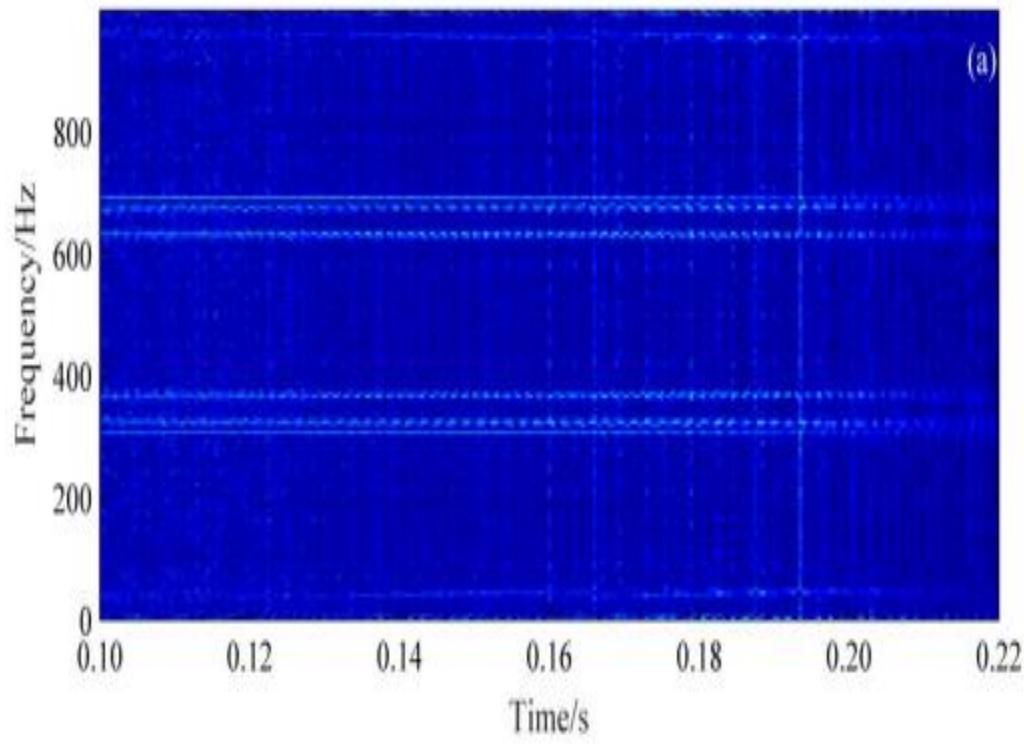
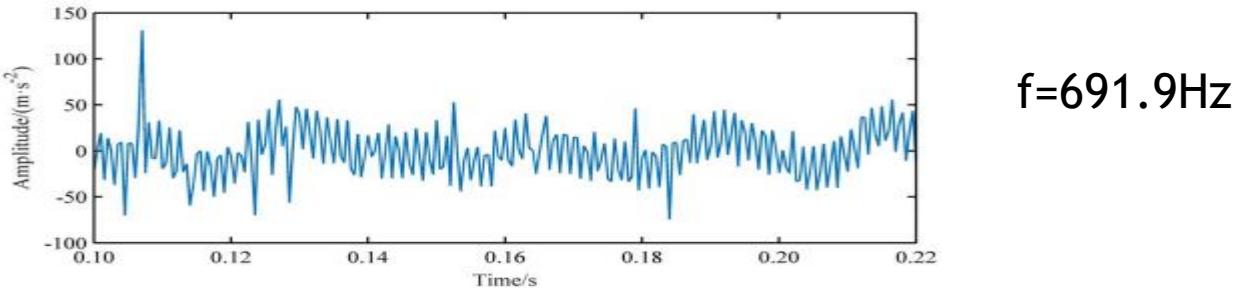
EMD

Results

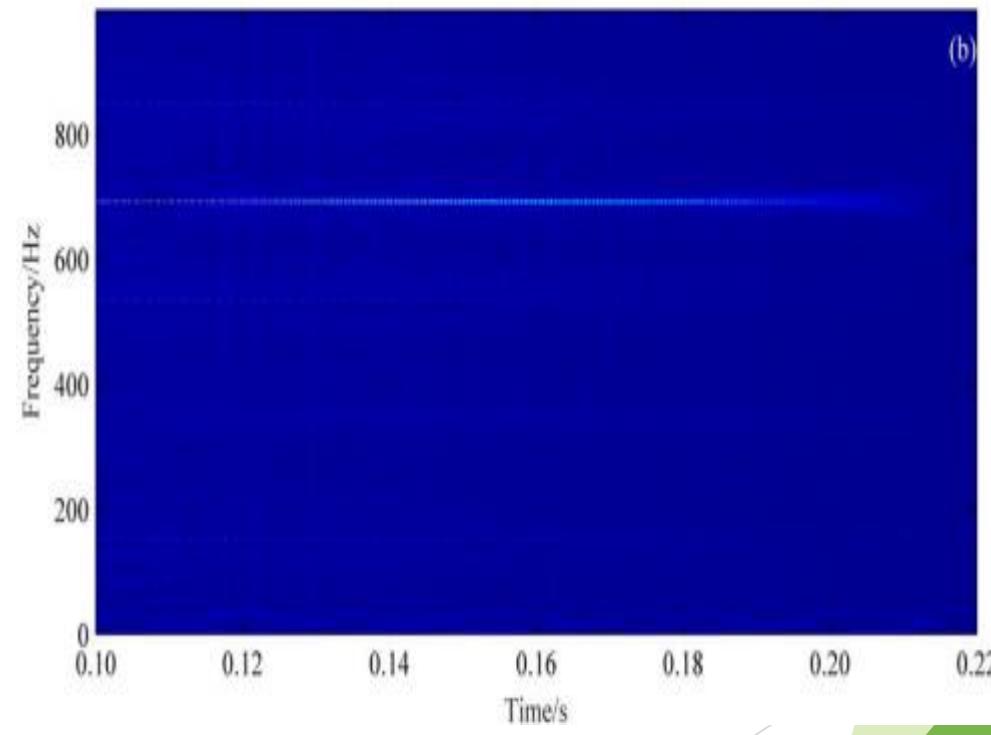


- ▶ 24th-order wheel polygon
- ▶ OOR amplitude: 0.02 mm
- ▶ $v = 300 \text{ km/h}$
- ▶ $R = 460 \text{ mm}$
- ▶ $f = \frac{v}{\lambda} = \frac{nv}{2\pi R} = 24 * \frac{300(\text{km/h})}{2\pi * 460(\text{mm})} = 691.9 \text{ Hz}$

Results

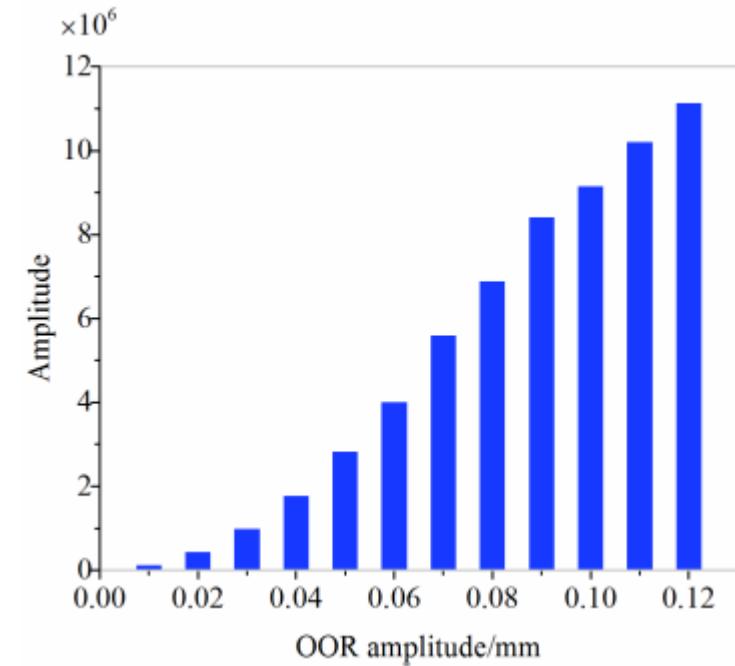
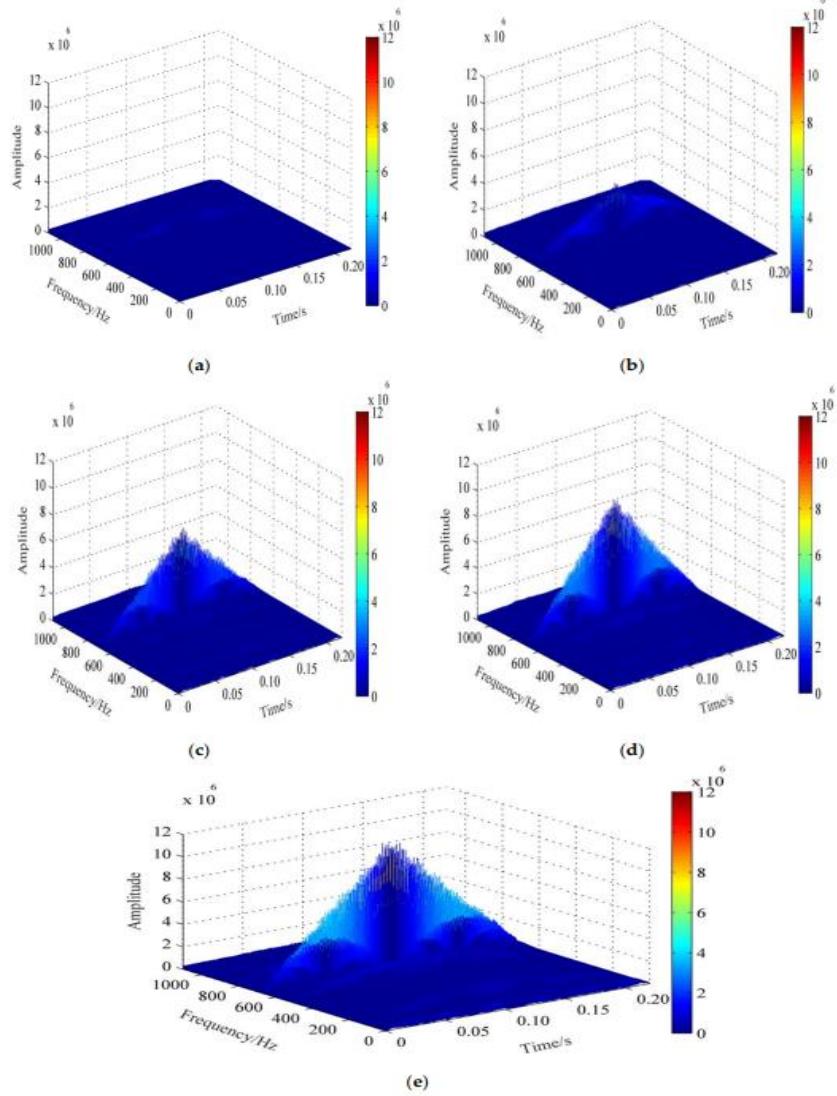


WVD

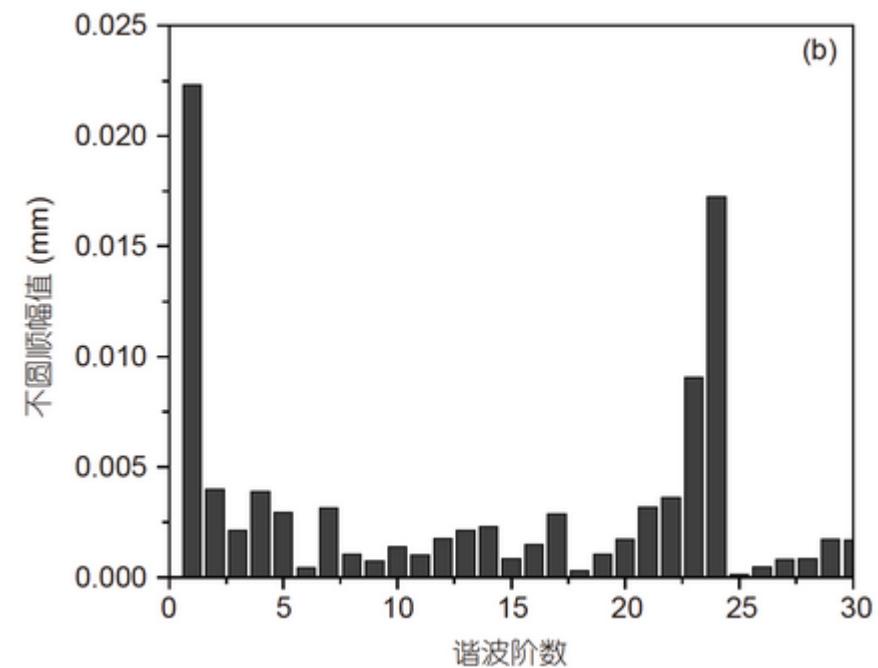
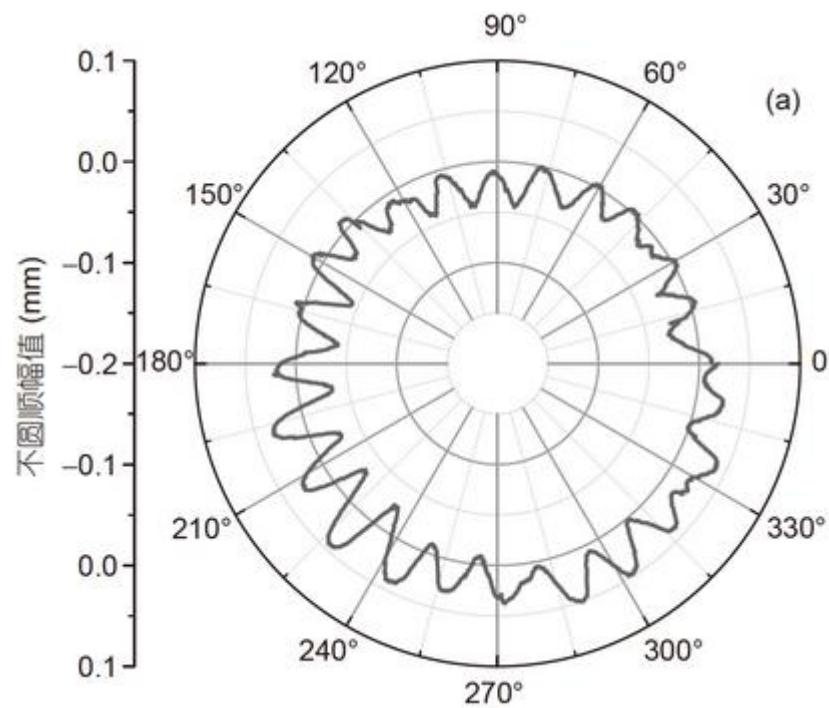


EEMD-WVD

Results—change OOR amplitude



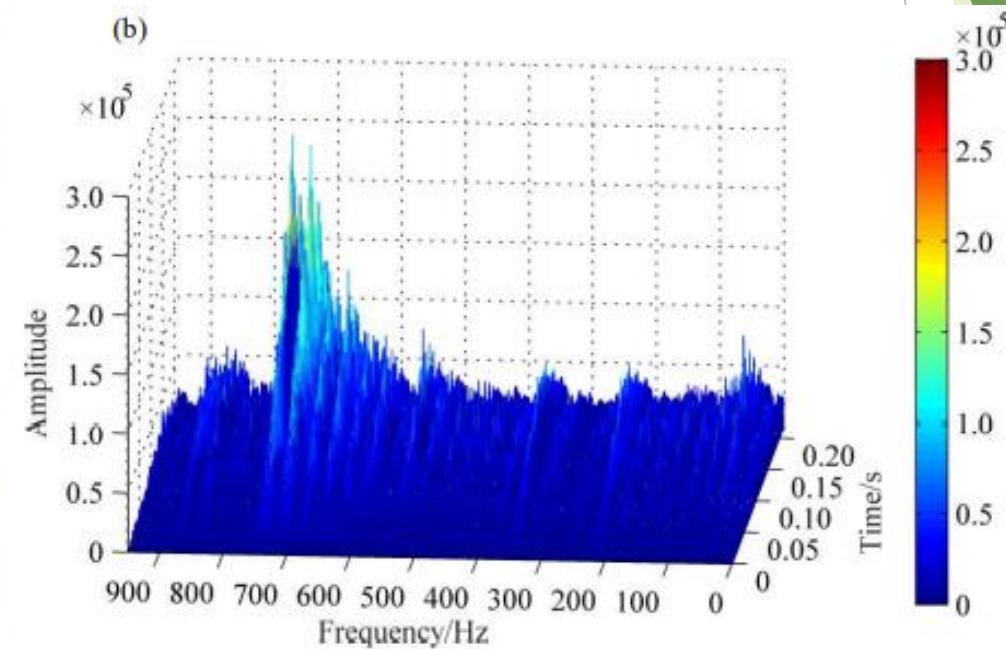
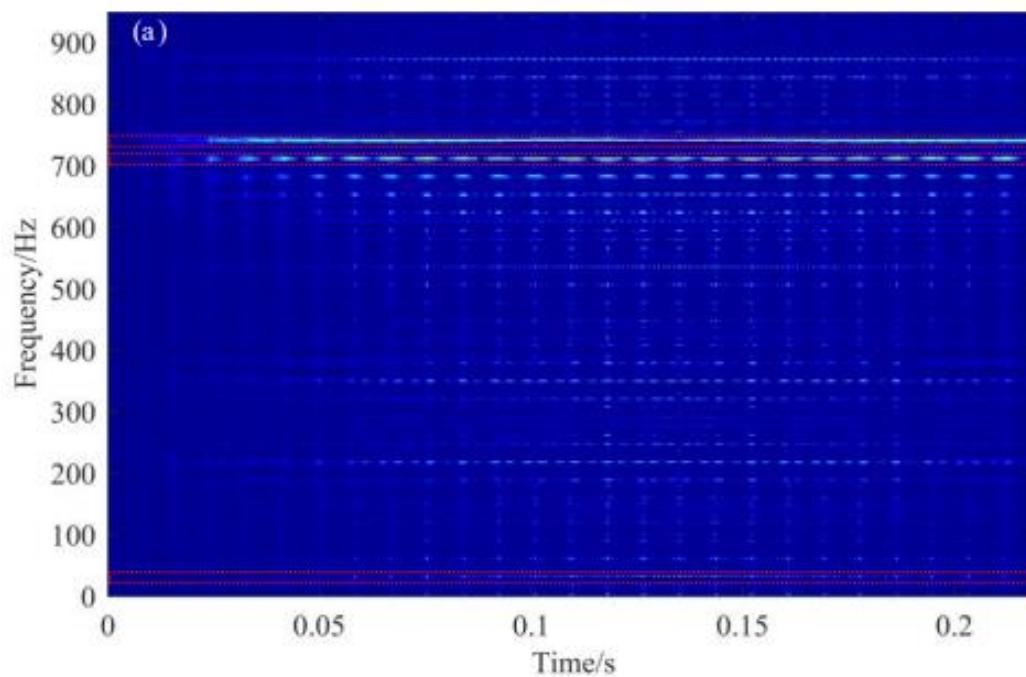
Results—real wheel



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From Reference [8]

Results—real wheel



Reference

- ▶ [1] Song Y., Liang L., Du Y., Sun B. (2020). Railway Polygonized Wheel Detection Based on Numerical Time-Frequency Analysis of Axle-Box Acceleration. *Applied Sciences*, 10(5), 1613.
- ▶ [2] P. Salvador, V. Naranjo, R. Insa and P. Teixeira, “Axebox accelerations: Their acquisition and time-frequency characterization for railway track monitoring purposes”, *Measurement*, vol. 82, pp. 301-302, Mar. 2016
- ▶ [3] Z. Li, M. Molodova, A. Nunez and R. Dollevoet, “Improvements in axle box acceleration measurements for the detection of light squats in railway infrastructure”, *IEEE Transactions on Industrial Electronics*, vol. 62, no. 7, pp.4387-4397, 2015.
- ▶ [4] J. C. Nielsen and A. Johansson, “Out-of-round railway wheels-a literature survey”, *Proc. Inst. Mech. Eng. F J. Rail Rapid Transit*, vol. 214, no. 2, pp. 79-91, 2000.
- ▶ [5] B. Liang, S. Iwnicki, A. Ball and A. E. Young, “Adaptive noise cancelling and time-frequency techniques for rail surface defect detection”, *Mechanical Systems and Signal Processing*, vol. 54, pp. 41-51, 2015.
- ▶ [6] 時頻分析與小波轉換 課程投影片
- ▶ [7] <https://zh.m.wikipedia.org/zh-tw/%E5%B8%8C%E7%88%BE%E4%BC%AF%E7%89%B9-%E9%BB%83%E8%BD%89%E6%8F%9B>
- ▶ [8] Chen, M., Zhai, W.M., et al., “Analysis of wheel-rail dynamic characteristics due to polygonal wheel passing through rail weld zone in high-speed railways”, *Sci. China Press* 64(25), 2573-2582, 2019. (in Chinese)